

Multilayered Oscillating Functional Surface

[0001] This application claims the benefit of U.S. Provisional Application No. 60/424,915 filed on November 8, 2002, entitled "Composite MEMS Micromirror Structure for High Frequency Operation Without Dynamic Deformation," which application is hereby incorporated herein by reference.

CROSS-REFERENCE TO RELATED APPLICATIONS

[0002] This application relates to the co-pending and commonly assigned patent application Serial No. _____, entitled "Multilayered Oscillating Device with Spine Support," (Attorney Docket TI-36490) filed concurrently herewith, which application is hereby incorporated herein by reference.

TECHNICAL FIELD

[0003] The present invention relates generally to rapidly moving functional surfaces, such as mirrors, and "scanning mirrors." More specifically, the invention relates to multilayered MEMS (micro-electric mechanical systems) torsional hinge functional surfaces, such as mirrors, operating at the resonance frequency of the device. A hinge layer having a first set of torsional hinges for providing the back and forth pivoting at a controlled frequency about a first axis includes an attaching member with a front side and a back side. A functional surface layer, such as a mirror, having a reflective surface is bonded or mounted to the front side of the hinge layer, and a back layer having a mass moment equal to the mass moment of the functional surface layer is bonded or mounted to the back side of the hinge layer. According to one embodiment, the mass moment of the front layer is the mass of the front layer times the distance or offset of the center of the mass of the front layer from the first axis and the mass moment of the back layer is

the mass of the back layer times the distance or offset of the center of the mass of the back layer from the first axis.

[0004] According to one embodiment, the hinge layer further comprises a second pair of torsional hinges for rapidly pivoting the functional surface of the device about a second axis to control movement in a direction substantially orthogonal to the pivoting movement about the first set of torsional hinges. When the functional surface of the device is a mirror, such mirrors are particularly suited for use as the drive engine for a laser printer and for generating a display on a screen. However, such mirrors may also be used to provide rapid switching in a fiber optic communication system.

BACKGROUND

[0005] Rotating polygon scanning mirrors are typically used in laser printers to provide a "raster" scan of the image of a laser light source across a moving photosensitive medium, such as a rotating drum. Such a system requires that the rotation of the photosensitive drum and the rotating polygon mirror be synchronized so that the beam of light (laser beam) sweeps or scans across the rotating drum in one direction as a facet of the polygon mirror rotates past the laser beam. The next facet of the rotating polygon mirror generates a similar scan or sweep which also traverses the rotating photosensitive drum but provides an image line that is spaced or displaced from the previous image line.

[0006] There have also been prior art efforts to use a less expensive flat mirror with a single reflective surface to provide a scanning beam. For example, a dual axis or single axis scanning mirror may be used to generate the beam sweep or scan instead of a rotating polygon mirror. The rotating photosensitive drum and the scanning mirror are synchronized as the drum rotates in

a forward direction to produce a printed image line on the medium that is at right angles or orthogonal with the beam scan or sweep generated by the pivoting mirror.

[0007] However, with single axis mirrors the return sweep will traverse a trajectory on the moving photosensitive drum that is at an angle with the printed image line resulting from the previous or forward sweep. Consequently, use of a single axis resonant mirror, according to the prior art, required that the modulation of the reflected light beam be interrupted as the mirror completed the return sweep or cycle, and then turned on again as the beam starts scanning in the original direction. Using only one of the sweep directions of the mirror, of course, reduces the print speed. Therefore, to effectively use an inexpensive scanning mirror to provide bi-directional printing, the prior art typically required that the beam scan move in a direction perpendicular to the scan such that the sweep of the mirror in each direction generates images on a moving or rotating photosensitive drum that are always parallel. This continuous perpendicular adjustment is preferably accomplished by the use of a dual axis torsional mirror, but could be accomplished by using a pair of single axis torsional mirrors. It has been discovered, however, at today's high print speeds both forward and reverse sweeps of a single axis mirror may be used, and that no orthogonal adjustment is necessary.

[0008] Texas Instruments presently manufactures torsional dual axis and single axis resonant mirror MEMS devices fabricated out of a single piece of material (such as silicon, for example) typically having a thickness of about 100 – 115 microns. The dual axis layout consists of a mirror normally supported on a gimbal frame by two silicon torsional hinges, whereas for a single axis mirror the mirror is supported directly by a pair of torsional hinges. The reflective surface may be of any desired shape, although an elliptical shape having a long axis of about 4.0 millimeters and a short axis of about 1.5 millimeters is particularly useful. The elongated

ellipse-shaped mirror is matched to the shape that the angle of the beam is received. The gimbal frame used by the dual axis mirror is attached to a support frame by another set of torsional hinges. These mirrors manufactured by Texas Instruments are particularly suitable for use as the scanning engine for high-speed laser printers and visual displays. These high-speed mirrors are also suitable for use as high-speed optical switches in communication systems. One example of a dual axis torsional hinged mirror is disclosed in U.S. Patent 6,295,154 entitled "Optical Switching Apparatus" and was assigned to the same assignee on the present invention.

[0009] The present invention is particularly applicable to a mirror or reflective surface supported by torsional hinges and the discussion and embodiments are primarily with respect to mirrors. However, as suggested by the title and the above discussion, the invention is also applicable to "functional surfaces" other than mirrors that have a need for high-speed pivoting or oscillations. Therefore, functional surfaces other than mirrors may include light gratings as well as surfaces not concerned with light beams and the movement of light beams.

[0010] Therefore, it will be appreciated that, although many references and embodiment in the specification are with respect to mirrors, the claims are not to be so limited except for such specific limitations in the claims.

[0011] According to the prior art, torsional hinge devices were initially driven directly by magnetic coils interacting with small magnets mounted on the pivoting device at a location orthogonal to and away from the pivoting axis to oscillate the device or, in the case of a mirror functional surface, create the sweeping movement of the beam. In a similar manner, orthogonal movement of a beam sweep was also controlled by magnetic coils interacting with magnets mounted on the gimbals frame at a location orthogonal to the axis used to pivot the gimbals frame.

[0012] According to the earlier prior art, the magnetic coils controlling the functional surface or reflective surface portion of a mirror typically received an alternating positive and negative signal at a frequency suitable for oscillating the device at the desired rate. Little or no consideration was given to the resonant pivoting frequency of the device. Consequently, depending on the desired oscillating frequency or rate and the natural resonant frequency of the device about the pair of torsional hinges, significant energy could be required to pivot the device and especially to maintain the functional surface of the device in a state of oscillation. Furthermore, the magnets mounted on the functional surface portion added mass and limited the oscillating speed.

[0013] Later torsional devices, such as mirrors, were manufactured to have a specific resonant frequency substantially equivalent to the desired oscillation rate. Such resonant frequency devices were particularly useful when the functional surface of the devices was a mirror used as a scanning engine. Various inertially coupled drive techniques including the use of piezoelectric devices and electrostatic devices have been used to initiate and keep the functional surface or mirror oscillations at the resonant frequency.

[0014] It has now been discovered that the earlier inexpensive and dependable magnetic drive can also be used and set up in such a way to both maintain the pivoting device at its resonant frequency and to provide orthogonal movement. Unfortunately, the added mass of the magnets becomes more and more of a problem as the required frequency increases to meet the higher and higher speed demands. Further, the functional surface of a device can be of almost any shape, including square, round, elliptical, etc. However, an elongated elliptical shape has been found to be particularly suitable if the functional surface is a mirror. Unfortunately, these elongated elliptical-shaped mirrors introduce moment of inertia forces that result in excess

flexing and bending of the mirror adjacent the hinges and tips of the mirror such that the mirror no longer meets the required "flatness" specifications for providing a satisfactory laser beam.

The thickness of the mirror may be increased to maintain the necessary flatness, but the added weight and mass results in excess stress on the torsional hinges which can cause failures and/or reduced life.

[0015] Therefore, a scanning device having sufficient stiffness to maintain acceptable flatness at high oscillation speeds would be advantageous.

SUMMARY OF THE INVENTION

[0016] The problems mentioned above are addressed by the present invention, which provides a multilayered pivoting or oscillating device. Pivoting or oscillating mirror embodiments of the invention may be used as the means of generating a sweeping or scanning beam of light across a photosensitive medium. The device comprises a hinge layer that defines an attaching member pivotally supported along a first axis by a first pair of torsional hinges extending to a support structure. The hinge layer has a front side and a back side. A functional layer is bonded to the front side of the attaching member. For example, according to one embodiment, a mirror layer having a reflection portion is bonded to the front side of the attaching member, and a back layer having a mass moment (of back layer) mass times back layer mass offset or distance from the first axis) substantially equal to the mass moment (mass of mirror layer times mirror layer mass offset or distance from the first axis) of the mirror layer (or other functional layer) is bonded to the back side of the attaching member. The back layer may be a permanent magnet if the pivoting drive is a magnetic drive. Alternately, the back layer may be another material, such as silicon, if the drive is an inertia coupled drive.

[0017] According to another embodiment, the hinge layer comprises a support member connected directly to the functional layer by the first pair of torsional hinges. Alternately, according to a dual axis embodiment, the hinge layer includes a second pair of torsional hinges extending between a support member and a gimbal portion arranged to allow the gimbal portion to pivot about a second axis substantially orthogonal to the first axis. The reflective surface portion is attached to the gimbal portion by the first pair of torsional hinges. When the functional surface of the device is a mirror, pivoting of the mirror along the first axis and about the first pair of torsional hinges results in a beam of light reflected from the reflective surface

sweeping back and forth, and pivoting about the second pair of torsional hinges results in the reflected light moving substantially orthogonal to the sweeping beam of light.

BRIEF DESCRIPTION OF THE DRAWINGS

[0018] Other objects and advantages of the invention will become apparent upon reading the following detailed description and upon referencing the accompanying drawings in which:

[0019] FIGs. 1A, 1B, and 1C illustrate the use of a rotating polygon mirror for generating the sweep of a laser printer according to the prior art;

[0020] FIGs. 2A and 2B are embodiments of a single axis scanning torsional hinge device wherein the functional surface is a mirror;

[0021] FIGs. 3A, 3B, 3C, and 3D illustrate a prior art example of using a single axis flat scanning mirror to generate a unidirectional beam sweep of a laser printer;

[0022] FIG. 4 is a perspective illustration of the single axis mirror of the type shown in FIG. 2A or 2B to generate the beam sweep of a laser printer;

[0023] FIGs. 5A and 5B are perspective views of two embodiments of prior art two-axis torsional hinge devices (such as mirrors) for generating a bi-directional movement of the functional surface;

[0024] FIGs. 6A, 6B, and 6C illustrate the use of one two-axis scanning mirror such as is shown in FIGs. 5A and 5B to generate a bi-directional beam sweep of a laser;

[0025] FIG. 7 illustrates one embodiment of a single axis magnetic drive;

[0026] FIGs. 8A and 8B show an exploded view and an assembled view of a magnetic drive multilayered scanning device according to the present invention when the functional surface is a scanning mirror;

[0027] FIG. 9 illustrates a single axis magnetic drive according to another embodiment;

[0028] FIGs. 10A, 10B and 10C illustrate the operation of a piezoelectric drive to create inertia coupled oscillations in a scanning functional surface;

[0029] FIGs. 11A and 11B show an exploded view and an assembled view of a piezoelectric driven multilayered device of the present invention;

[0030] FIGs. 12A and 12B show an exploded view and an assembled view of a magnetic driven dual axis multilayered high-speed device when the functional surface is a mirror; and

[0031] FIGs. 13A and 13B show an exploded view and an assembled view of a piezoelectric driven dual axis multilayered high-speed device when the functional surface is a mirror.

DETAILED DESCRIPTION OF ILLUSTRATIVE EMBODIMENTS

[0032] Like reference numbers in the figures are used herein to designate like elements throughout the various views of the present invention. The figures are not intended to be drawn to scale and in some instances, for illustrative purposes, the drawings may intentionally not be to scale. One of ordinary skill in the art will appreciate the many possible applications and variations of the present invention based on the following examples of possible embodiments of the present invention. The present invention relates to a high-speed pivoting device, such as a mirror, with a moveable reflecting surface that is suitable for providing the raster scans for laser printers and displays or high-speed optical switching. More specifically, the invention relates to a pivoting device and a magnetic drive for maintaining high speed resonant pivoting of the functional surface about a pair of torsional hinges.

[0033] Referring now to FIGs. 1A, 1B and 1C, there is shown an illustration of the operation of a prior art printer using a rotating polygon mirror. As shown in FIG. 1A, there is a rotating polygon mirror 10 which in the illustration has eight reflective surfaces 10a – 10h. A light source 12 produces a beam of light 14a, such as a laser beam, that is focused on the rotating polygon mirror so that the beam of light from the light source 12 is intercepted by the facets 10a – 10h of rotating polygon mirror 10. Thus, the laser beam of light 14a from the light source 12 is reflected from the facets 10a – 10h of the polygon mirror 10 as illustrated by dashed line 14b to a moving photosensitive medium 16 such as a rotating photosensitive drum 18 having an axis of rotation 20. The moving photosensitive medium 16 or drum 18 rotates around axis 20 in a direction as indicated by the arcuate arrow 22 such that the area of the moving photosensitive medium 16 or drum 18 exposed to the light beam 14b is continuously changing. As shown in FIG. 1A, the polygon mirror 10 is also rotating about an axis 24 (axis is perpendicular to the

drawing in this view) as indicated by the second accurate arrow 26. Thus, it can be seen that the leading edge 28 of facet 10b of rotating polygon mirror 10 will be the first part of facet 10b to intercept the laser beam of light 14a from the light source 12. As the mirror 10 rotates, each of the eight facets of mirror 10 will intercept the light beam 14a in turn. As will be appreciated by those skilled in the art, the optics to focus the light beam, the lens system to flatten the focal plane to the photosensitive drum, and any fold mirrors to change the direction of the scanned beam are omitted for ease of understanding.

[0034] Illustrated below the rotating polygon mirror 10 is a second view of the photosensitive medium 16 or drum 18 as seen from the polygon scanner. As shown by the photosensitive drum view 18, there is the beginning point 30 of an image of the laser beam 14b on drum 18 immediately after the facet 10b intercepts the light beam 14a and reflects it to the moving photosensitive medium 16 or drum 18.

[0035] Referring now to FIG. 1B, there is shown substantially the same arrangement as illustrated in FIG. 1A except the rotating polygon mirror 10 has continued its rotation about axis 24 such that the facet 10b has rotated so that its interception of the laser beam 14a is about to end. As will also be appreciated by those skilled in the art, because of the varying angle the mirror facets present to the intercepted light beam 14a, the reflected light beam 14b will move across the surface of the rotating drum as shown by arrow 32 and dashed line 34 in FIG. 1B.

[0036] However, it will also be appreciated that since rotating drum 18 was moving orthogonally with respect to the scanning movement of the light beam 14b, that if the axis of rotation 24 of the rotating mirror was exactly orthogonal to the axis 20 of the rotating photosensitive drum 18, an image of the sweeping or scanning light beam on the photosensitive drum would be recorded at a slight angle. As shown more clearly by the lower view of the

photosensitive drum 18, dashed line 34 illustrates that the trajectory of the light beam 14b is itself at a slight angle, whereas the solid line 36 representing the resulting image on the photosensitive drum is not angled but orthogonal to the rotation or movement of the photosensitive medium 16. To accomplish this parallel printed line image 36, the rotating axis 24 of the polygon mirror 10 is typically mounted at a slight tilt with respect to the rotating photosensitive drum 18 so that the amount of vertical travel or distance traveled by the light beam along vertical axis 38 during a sweep or scan across medium 16 is equal to the amount of movement or rotation of the photosensitive medium 16 or drum 18. Alternately, if necessary, this tilt can also be accomplished using a fold mirror that is tilted.

[0037] FIG. 1C illustrates that facet 10b of rotating polygon mirror 10 has rotated away from the light beam 14a, and facet 10c has just intercepted the light beam. Thus, the process is repeated for a second image line. Continuous rotation will of course result in each facet of rotating mirror 10 intercepting light beam 14a so as to produce a series of parallel and spaced image lines, such as image line 36a, which when viewed together will form a line of print or other image.

[0038] It will be further appreciated by those skilled in the laser printing art, that the rotating polygon mirror is a very precise and expensive part or component of the laser printer that must spin at terrific speeds without undue wear of the bearings even for rather slow speed printers. Therefore, it would be desirable if a less complex flat mirror, such as for example a resonant flat mirror, could be used to replace the complex and heavy polygonal scanning mirror.

[0039] FIGs. 2A and 2B illustrate prior art single layer, single axis torsional devices where the functional surfaces are mirrors. Each of the mirrors of FIGs. 2A and 2B include a support member 40 supporting a mirror or reflective surface 42, which may be substantially any shape

but for many applications the elongated ellipse shape of FIG. 2B is preferred. The functional surface, or mirror, is supported by a single pair of torsional hinges 44a and 44b. Thus, it will be appreciated that, when the functional surface is a mirror, if the mirror portion 42 can be maintained in an oscillation state around axis 46 by a drive source, the mirror can be used to cause a sweeping light beam to repeatedly move across a photosensitive medium, or to rapidly switch a light beam to a selected one of a plurality of optical fibers.

[0040] It will also be appreciated that an alternate embodiment of a single axis mirror or other functional surface may not require the support member or frame 40 as shown in FIGs. 2A and 2B. For example, as shown in both figures, the torsional hinges 44a and 44b may simply extend to a pair of hinge anchor pads 48a and 48b as shown in dotted lines. The functional surface or, in the present example, mirror portion 42, is suitably polished on its upper surface to provide a specular or mirror surface.

[0041] The prior art single layered devices were typically MEMS (micro-electric mechanical systems) type devices manufactured from a slice of single crystal silicon. Further, because of the advantageous material properties of single crystalline silicon, such MEMS based devices have a very sharp torsional resonance. The Q of the torsional resonance typically is in the range of 100 to over 1000. This sharp resonance results in a large mechanical amplification of the device's motion at a resonance frequency versus a non-resonant frequency. Therefore, it is typically advantageous to pivot the device about the scanning axis at the resonant frequency. This dramatically reduces the power needed to maintain the device in oscillation.

[0042] There are many possible drive mechanisms available to provide the oscillating movement about the scan axis. For example, FIG. 2A illustrates a prior art magnetic drive device wherein the functional surface is a mirror having a pair of permanent magnets 50a and

50b mounted on tabs 52a and 52b respectively. The permanent magnets 50a and 50b interact with a pair of coils (not shown) located below the mirror structure. The mirror mechanical motion in the scan axis is typically required to be greater than 15 degrees and may be as great as 30 degrees. Resonant drive methods involve applying a small rotational motion at or near the resonant frequency of the functional surface directly to the torsionally hinged device, or alternately motion at the resonant frequency may be applied to the whole silicon structure, which then excites the device to resonantly pivot or oscillate about its torsional axis. In inertial resonant type of drive methods a very small motion of the whole silicon structure can excite a very large rotational motion of the device. Suitable inertial resonant drive sources include piezoelectric drives and electrostatic drive circuits. A magnetic resonant drive that applies a resonant magnetic force directly to the torsional hinged functional surface portion has also been found to be suitable for generating the resonant oscillation for producing the back and forth beam sweep when the functional surface is a mirror.

[0043] Further, by carefully controlling the dimension of hinges 44a and 44b (i.e., width, length and thickness) the device may be manufactured to have a natural resonant frequency which is substantially the same as the desired pivoting speed or oscillating frequency of the device. Thus, by providing a functional surface, such as a mirror, with a high-speed resonant frequency substantially equal to the desired pivoting speed or oscillating frequency, the power loading may be reduced.

[0044] Referring now to FIGs. 3A, 3B, 3C and 3D, there is illustrated a prior art example of a laser printer using a single-axis oscillating mirror to generate the beam sweep. As will be appreciated by those skilled in the art and as illustrated in the following figures, prior art efforts have typically been limited to only using one direction of the oscillating beam sweep because of

the non-parallel image lines generated by the return sweep. As shown in FIGs. 3A, 3B, 3C and 3D, the arrangement is substantially the same as shown in FIGs. 1A, 1B and 1C except that the rotating polygon mirror has been replaced with a single oscillating flat mirror 54 that oscillates in both directions as indicated by double headed arcuate arrow 56. As was the case with respect to FIG. 1A, FIG. 3A illustrates the beginning of a beam sweep at point 30 by the single axis mirror 54. Likewise, arrow 32 and dashed line 34 in FIG. 3B illustrate the direction of the beam sweep as mirror 54 substantially completes its scan as it rotates in a direction as indicated by arrow 56a. Referring to the lower view of the photosensitive drum 18, according to this prior art embodiment, the mirror 54 is mounted at a slight angle such that the beam sweep is synchronized with the movement of the rotating drum 18 so that the distance the medium moves is equal to the vertical distance the light beam moves during a sweep. As was the case for the polygon mirror of FIG. 1B, the slightly angled trajectory as illustrated by dashed line 34 results in a horizontal image line 36 on the moving photosensitive medium 16 or drum 18.

[0045] Thus, up to this point, it would appear that the flat surface single torsional axis oscillating mirror 54 should work at least as well as the rotating polygon mirror 10 as discussed with respect to FIGs. 1A, 1B, and 1C. However, when the oscillating mirror starts pivoting back in the opposite direction as shown by the arcuate arrow 56b, with prior art scanning mirror printers, it was necessary to turn the beam, indicated by dashed line 34a in FIG. 3C, off and not print during the return sweep since the vertical movement of the mirror resulting from being mounted at a slight angle and the movement of the moving photosensitive medium 16 or rotating drum 18 were cumulative rather than subtractive. Consequently, if used for printing, the angled trajectory 34a of the return beam combined with movement of the rotating drum 18 would result in a printed image line 36a which is at even a greater angle than what would occur simply due to

the movement of the rotating photosensitive drum 18. This, of course, is caused by the fact that as the beam sweep returns, it will be moving in a downward direction as indicated by arrow 58 rather than an upward direction, whereas the photosensitive drum movement is in the upward direction indicated by arrow 60. Thus, as stated above, the movement of the drum and the beam trajectory are cumulative. Therefore, for satisfactory printing by a resonant scanning mirror printer according to the prior art, it was understood that the light beam and the printing were typically interrupted and/or stopped during the return trajectory of the scan. Thus, the oscillating mirror 54 was required to complete its reverse scan and then start its forward scan again as indicated at 30A, at which time the modulated laser was again turned on and a second image line printed as indicated in FIG. 3D.

[0046] FIG. 4 illustrates a perspective illustration of a scanning mirror used to generate an image on a medium 16. The mirror device 56, such as the single axis mirror shown in FIGs. 2A and 2B, pivots about a single axis so that the reflecting surface 42 of the mirror device 56 receives the light beam 14a from source 12 and provides the right to left and left to right beam sweep 14b between limits 64 and 66 as was discussed with respect to FIGs. 3A, 3B, 3C and 3D. This left to right and right to left beam sweep provides the parallel lines 68 and 70 as the medium 16 moves in the direction indicated by arrow 72.

[0047] It will also be appreciated that various shapes of a functional surface can be used in the practice of this invention. Further, in the case of a scanning mirror, the demand for higher and higher print speeds will require a higher and higher oscillation speed. Similarly, high-speed pivoting is also necessary when the functional surface is a mirror used as high-speed optical switch. However, in addition to high-speed pivoting of the device, it is also important that the functional surface not deform as it pivots at high speed. More specifically, if the functional

surface is a scanning mirror, it is important that the mirror not deform as it sweeps the laser beam across the photosensitive medium during a scan cycle. One way to avoid flexing or deforming of the rapidly pivoting functional surface or mirror is to increase the thickness of the functional surface. Unfortunately, increasing the device thickness results in increased stress on the torsional hinges due to an increase in weight, mass and moment of inertia.

[0048] Referring now to FIGs. 5A and 5B, there is shown a perspective view and a top view, respectively, of two bi-directional assemblies wherein the functional surfaces are mirrors. Such dual axis mirrors may be used to provide a high-speed beam sweep wherein the high-speed beam sweep is also adjusted in a direction orthogonal to the beam sweep of the mirror. When used as a scanning engine for a printer, adjusting the beam sweep orthogonally allows the printed image lines produced by a beam sweep in one direction and then in a reverse direction to be maintained parallel to each other. As shown, the moveable assemblies of both FIGs. 5A and 5B are illustrated as being mounted on a support 74, and suitable for being driven along both axes 46 and 76. As was discussed above with respect to single axis resonant devices, the assembly may be formed from a substantially planar material and the functional or moving parts may be etched in the planar sheet of material (such as silicon) by techniques similar to those used in semiconductor art. As shown, the functional components include a support member or frame portion 40, similar to the single axis device discussed above. However, unlike the single axis resonant device, the support structure of the dual axis device also includes an intermediate gimbals portion 78 as well as the functional surface or mirror portion 42. It will be appreciated that the intermediate gimbals portion 78 is hinged to the support member or frame portion 40 at two ends by a pair of torsional hinges 80a and 80b spaced apart and aligned along an axis 76. Except for the pair of hinges 80a and 80b, the intermediate gimbals portion 78 is separated from

the frame portion 40. It should also be appreciated that, although support member or frame portion 40 provides an excellent support for attaching the device to support structure 74, it may be desirable to eliminate the frame portion 40 and simply extend the torsional hinges 80a and 80b and anchor the hinges directly to the support 74 as indicated by anchors 82a and 82b shown in dotted lines on FIGs. 5A and 5B.

[0049] The inner, centrally disposed functional surface, such as mirror portion 42, is attached to gimbals portion 78 at hinges 44a and 44b along an axis 46 that is orthogonal to or rotated 90° from axis 76. The reflective surface or mirror portion 42 is suitably polished on its upper surface to provide a specular or mirror surface. If desired, a coating of suitable material can be placed on the mirror portion to enhance its reflectivity for specific radiation wavelengths.

[0050] As was mentioned above with respect to single axis devices, there are many combinations of drive mechanisms for the scan or sweep axis. For the cross scan or orthogonal axis, since the angular motion required is usually much less, an electromagnetic drive may be used to produce a controlled movement about the torsional hinges 80a and 80b to orthogonally move and position the beam sweep to a precise position. Consequently, a set of permanent magnet sets 84a and 84b may be associated with the movement about hinges 80a and 80b.

[0051] FIGs. 6A, 6B and 6C illustrate the use of a dual axis scanning resonant mirror such as shown in FIGs. 5A and 5B as a scanning engine for a laser printer. As can be seen from FIGs. 6A and 6B, the operation of a dual axis scanning mirror assembly 86 as it scans from right to left in the figures is substantially the same as mirror 56 pivoting around a single axis as discussed and shown in FIGs. 3A-3D. However, unlike the single axis mirror 56 and as shown in FIG. 6C, it is not required to turn the laser (light beam 14b) off during the return scan, since a return or left to right scan in FIG. 6C can be continuously modulated during the return scan so as to produce a

printed line or image on the moving photosensitive medium 16. The second printed line of images, according to the present invention, will be parallel to the previous right to left scan. This is, of course, accomplished by slight pivoting of the mirror 86 around orthogonal axis 76 of the dual axis mirror as was discussed above.

[0052] Further, as was discussed above with respect to a single axis mirror, by carefully controlling the dimension of hinges 44a and 44b (i.e., width, length and thickness) illustrated in FIGs. 5A and 5B, the device may be manufactured to have a natural resonant frequency which is substantially the same as the desired oscillating frequency of the device. Thus, when the functional surface is a mirror, by providing the mirror with a resonant frequency substantially equal to the desired oscillating frequency, the power loading may be reduced.

[0053] From the above discussion, it will be appreciated that it is advantageous to manufacture a scanning device having a mirror as the functional surface for use as a drive engine for a visual display or printer and that the mirror have a resonant frequency substantially the same as the desired raster or sweep frequency of the printer or display. As was also discussed, a magnetic drive is an inexpensive, dependable and effective technique for starting and maintaining the oscillating functional surface, or mirror, at its resonant frequency.

Unfortunately, the magnet sets 50a and 50b located on tabs 52a and 52b of the functional surface of FIG. 5A adds to the mass and moment of inertia of the resonant device, which in turn tends to reduce the resonant frequency of the device. For example, the resonant frequency of one dual axis magnetic drive device of the type shown in FIG. 5A is about 100 Hz and would be even lower if the size of the mirror or functional surface was increased. A speed of 100 Hz simply is not fast enough for many if not most mirror applications. Therefore a structure with a magnetic drive and increased resonant frequency would be advantageous.

[0054] Referring now to FIG. 7, there is a simplified illustration of a pivoting functional surface 88 (such as the mirror shown in FIGs. 8A and 8B) and a permanent magnet arrangement that significantly reduces the inertia forces of the apparatus. As shown in FIGs. 8A and 8B, the tabs 52a and 52b of FIG. 5A used to mount the permanent magnet sets 50a and 50b have been eliminated and a single magnet 90 is mounted behind the mirror 88. According to the embodiment shown in FIG. 7, magnet 90 has a diametral charge perpendicular to the axis of rotation, as illustrated by double headed arrow 94, rather than an axial charge. It will, of course, also be necessary to relocate the drive coil 96 so that it is substantially below magnet 90.

[0055] FIG. 9 shows a second magnetic drive arrangement. As shown, an axial charged magnet 100 is used instead of the diametral charged magnet of FIG. 7. Further, the coil 96 shown in FIG. 7 is replaced by an electro magnet device, such as device 102, having legs 104a and 104b, that extend to each side of the magnet 100. Thus, alternating current applied to coil 105 results in the magnetic field at the tips of legs 104a and 104b continuously changing polarity. This change in polarity creates alternating push-pull forces on magnet 100.

[0056] As also mentioned above, an inertially coupled resonant drive system may also be used to create resonant pivotal oscillation of the scanning device. FIGs. 10A, 10B and 10C illustrate an arrangement of an inertially coupled piezoelectric drive. FIGs. 10A and 10B show a top view and a side view respectively of a single axis torsional hinged device wherein a mirror is the functional surface. As shown, the mirror uses piezoelectric elements to drive a mirror of the type shown in FIGs. 11A and 11B and to be discussed below, to resonance. As shown in FIGs. 10A and 10B, the apparatus includes a support frame 106 having two long sides 108a and 108b and two short sides 110a and 110b. The short side 110a is mounted to support structure 112 by means of stand-off 114. The mirror or functional surface portion 115 is attached to short sides

110a and 110b by the torsional hinges 116a and 116b such that the oscillating portion 115 is located above a cavity 118 in support structure 112. Slices of piezoelectric material 120a and 120b are bonded to long sides 108a and 108b of the support frame 106 as shown. The slices of piezoelectric material are sliced so that they bend or curve when a voltage is applied across the length of the strip or slice of material. As will be appreciated by those skilled in the art of piezoelectric materials, the response time is extremely fast such that an alternating voltage even having a frequency as high as between 2-25 KHz will cause the material to bend and flex at the same frequency as the applied voltage. Therefore, since the slices of piezoelectric material are bonded to the support frame of the device, the application of an alternating voltage through conductors or wires 122a and 122b from the AC voltage source 124 and having a frequency substantially equal to the resonant frequency of the oscillating portion 115 as shown in FIG. 10C will cause vibration motion to be inertially coupled to the oscillating portion 115 of the device and thereby initiate and maintain the device in resonant pivoting oscillation.

[0057] The arrangement of piezoelectric slices discussed with respect to FIGs. 10A, 10B and 10C is for example only and other arrangements may be equally suitable for generating resonant motion.

[0058] Thus, from the above discussion it will be appreciate that although all types of high-speed devices, such as scanning mirrors, may be used in high-speed optical switches as well as various printer and display applications, resonant scanning mirrors having elongated elliptical shapes in the direction of rotation so that the light beam can be reflected from the mirror surface as long as possible may be the most cost effective and suitable for use in high speed printers and displays. Further, mirrors used for high-speed optical switches are preferably designed to have a resonant frequency that is equal to the desired pivoting speed of the optical switches to help

reduce power loading. However, elongated functional surfaces, such as these elongated elliptical shaped mirrors, introduce a new set of problems and concerns when pivoting at high speed.

[0059] For example, such elongated elliptical mirrors are typically manufactured from a slice of single crystal silicon. At the same time, to achieve the very high resonant oscillation and hinge flexibility necessary to obtain sufficient rotational movement, it is necessary that the torsional hinges be very thin. Unfortunately, if the slice of single crystal silicon is sufficiently thin to fabricate torsional hinges that operate at high oscillating speeds, the structure may be too flexible to use as the reflecting surface of a mirror device. At high pivoting speeds, the tips of an elongated elliptical mirror travel at very high speeds and gain significant inertia. Consequently, the functional surface, or mirror, tends to flex excessively. This excessive flexing of course means that during some portions of the oscillating cycle, the device bends or flexes and is not flat. This means, for many mirror applications the mirror has too much curvature or flex during the oscillating cycle. This variation in mirror flatness at high frequencies is simply unacceptable for many displays, printers and optical switching applications.

[0060] One attempt at solving the conflict between the need for flexible hinges and a rigid or flat reflecting surface is the use of an additional layer of material to support the functional surface (such as for example, a mirror). Therefore, referring again to FIGs. 8A and 8B, there is shown an exploded view and an assembled view of a single axis multilayered scanning device having a mirror as the functional surface. As shown, the multilayered scanning device comprises a support structure or hinge layer 126 for pivotally supporting an attaching member 128 having a front side 130 and a back side 132 connected to an anchor member 134 by a pair of torsional hinges 136a and 136b. According to this embodiment, anchor member 134 is a frame as shown. However, according to another embodiment, anchor member 134 could be replaced by a pair of

anchor pads 138a and 138b as indicated by the dotted lines. The operational or functional portion 92 is typically thicker than the hinge layer 126 and has a front portion 140. When the functional surface is a mirror, the front portion 140 has a reflecting surface 142 and a back portion 144. The back portion 144 is bonded or mounted to the front side 130 of the attaching member 128 and a back layer such as permanent magnet 90 is bonded or mounted to the back side 132 of the attaching member 128. As shown, permanent magnet 90 is bonded along the axis 146 to the center of the back side 132 of attaching member 128. Permanent magnet 90 is considerably stiffer than the hinge layer 124 and functional surface portion 92 and consequently stiffens and reinforces the structure in the middle area where the magnet is located. The mass moment of the permanent magnet 90 (mass of permanent magnet 90 times the offset of the center of mass of the permanent magnet 90 from axis 146) is selected to be substantially equal to, and opposite the mass moment of the functional surface portion 92 (mass of functional surface portion 92 times the offset of the center of mass of functional surface portion 92 from axis 146) such that the moment of inertia of the assembled multilayered torsional hinged device (or mirror) is centered on the axis of rotation extending through hinges 136a and 136b. More specifically, according to one embodiment of the invention, the mass moment of the functional surface or mirror layer is the product of the mass functional surface or mirror layer times the offset or distance of the center of mass of the functional surface from the axis of rotation, and the mass moment of the back layer is the product of the mass of the back layer times the offset or distance of the center of mass of the back layer from the axis of rotation. FIG. 8B shows the assembled structure. The functional surface portion 92 and permanent magnet 90 of the assembled structure of FIG. 8B, of course add significant weight that must be supported by the torsional hinges 136a and 136b. Therefore, to assure that the hinges are not under excessive stress, the design of the

torsional hinges must consider the stress caused by the inertia forces and the added weight to avoid unacceptable failure rates and short life.

[0061] In addition to an oscillating device having a magnetic drive, such as the mirror device shown in FIGs. 8A and 8B, the basic concepts of the embodiments discussed with respect to these figures are also applicable to resonant devices using inertia drive such as provided by a piezoelectric device as discussed above. Therefore, referring again to FIGs. 11A and 11B, there is shown an exploded view and an assembled view of a multilayered resonant device suitable for use with a piezoelectric drive. Those elements of the structure that are equivalent to the elements of FIGs. 8A and 8B carry the same reference numbers. Therefore, as shown, the embodiment of FIGs. 11A and 11B differs with respect to FIGs. 8A and 8B only in the presence of a back layer 156 made of a material such as silicon rather than the permanent magnet 90. However, as was the case for the embodiment of FIGs. 8A and 8B, the back layer 156 is also selected to have a mass moment (mass of back layer 156 times the offset of the center of the mass of back layer 156 from axis 146) equal to the mass moment of the functional surface portion 92 (mass of functional surface portion 92 times the offset of the center of the mass functional surface portion 92 from axis 146).

[0062] Likewise, FIGs. 12A and 12B show a dual axis multilayered magnetic drive resonant device having a mirror as the functional surface. This embodiment is substantially the same as that discussed with respect to FIGs. 8A and 8B except that the support structure or hinge layer 126a further defines the gimbals portion 158 which pivots orthogonally to the functional surface portion along torsional hinges 160a and 160b and about axis 162.

[0063] Similarly, FIGs. 13A and 13B are similar to the embodiments shown in FIGs. 12A and 12B except that the support structure or hinge layer 126a further defines the gimbals portion

158, which pivots orthogonal to the functional surface along torsional hinges 160a and 160b and about axis 162.

[0064] Each of the assembled dual axis devices illustrated by FIGs. 12B and 13B include a back portion (whether a permanent magnet 90 or piece of silicon 156) that, once attached to the attaching member 132, has a mass moment as defined above that is substantially equal to the mass moment of the functional surface portion 92 also defined above. Consequently, any moment of inertia of the device resulting from these added portions is centered on the two axes of rotation.

[0065] The foregoing descriptions of specific embodiments of the present invention have been presented for purposes of illustration and description. They are not intended to be exhaustive or to limit the invention to the precise forms disclosed as many modifications and variations are possible in light of the above teaching. The embodiments were chosen and described in order to best explain the principles of the invention and its practical application to thereby enable others skilled in the art to best utilize the invention and various embodiments with various modifications as are suited to the particular use contemplated. It is intended that the scope of the invention be defined by the claims appended hereto and their equivalents.